

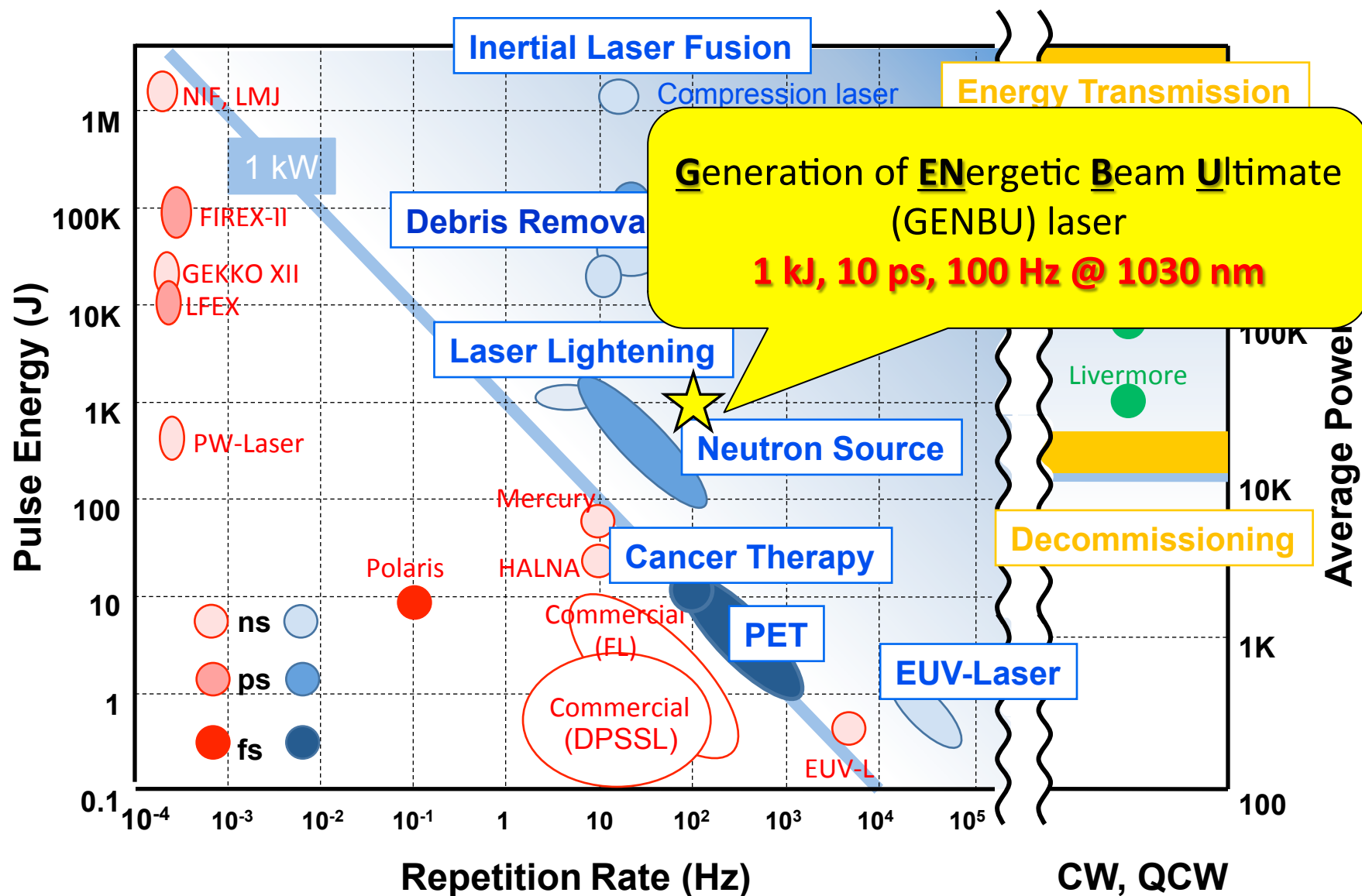
# Thermal analysis of cryogenic Yb:YAG TRAM laser for high-average power systems

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# Applications for Next Generation High Energy Lasers



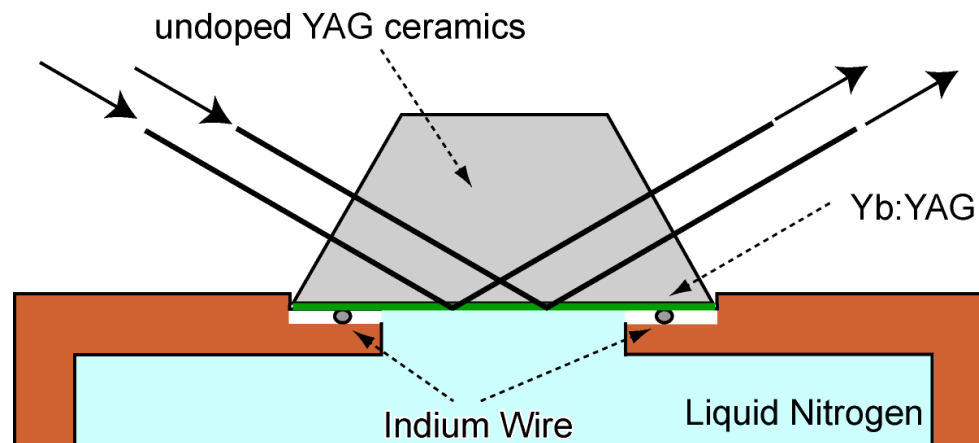
# Introduction

Objective: **Output power  $> 10$  kW**, High Efficiency, High Quality

Issues: **Thermal Problems**, Damage, etc...

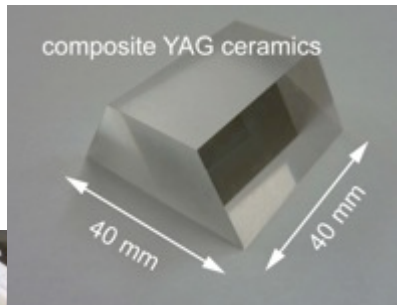
Approaches:

- **Cryogenic Yb:YAG Ceramics ( $< 100$  K)**
  - Efficient 4-level operation, improved thermal properties
- **Total-Reflection Active-Mirror (TRAM)**
  - Without HR coating,  $\text{LN}_2$  directly cooling



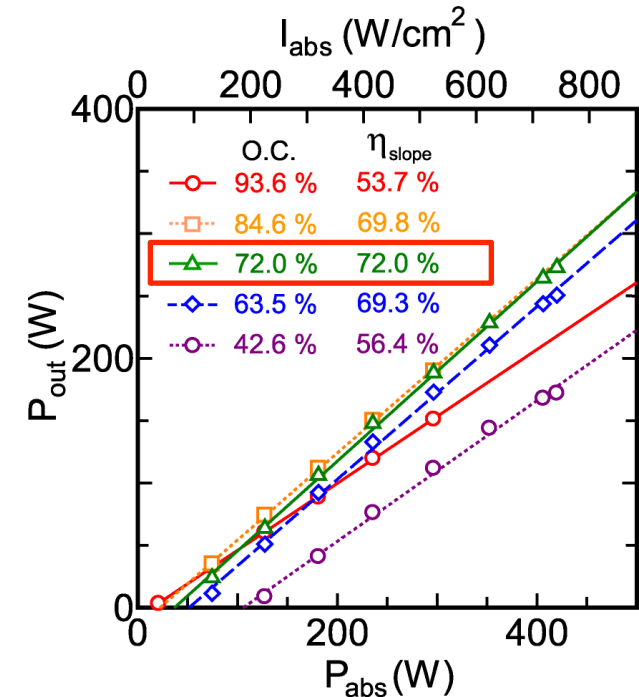
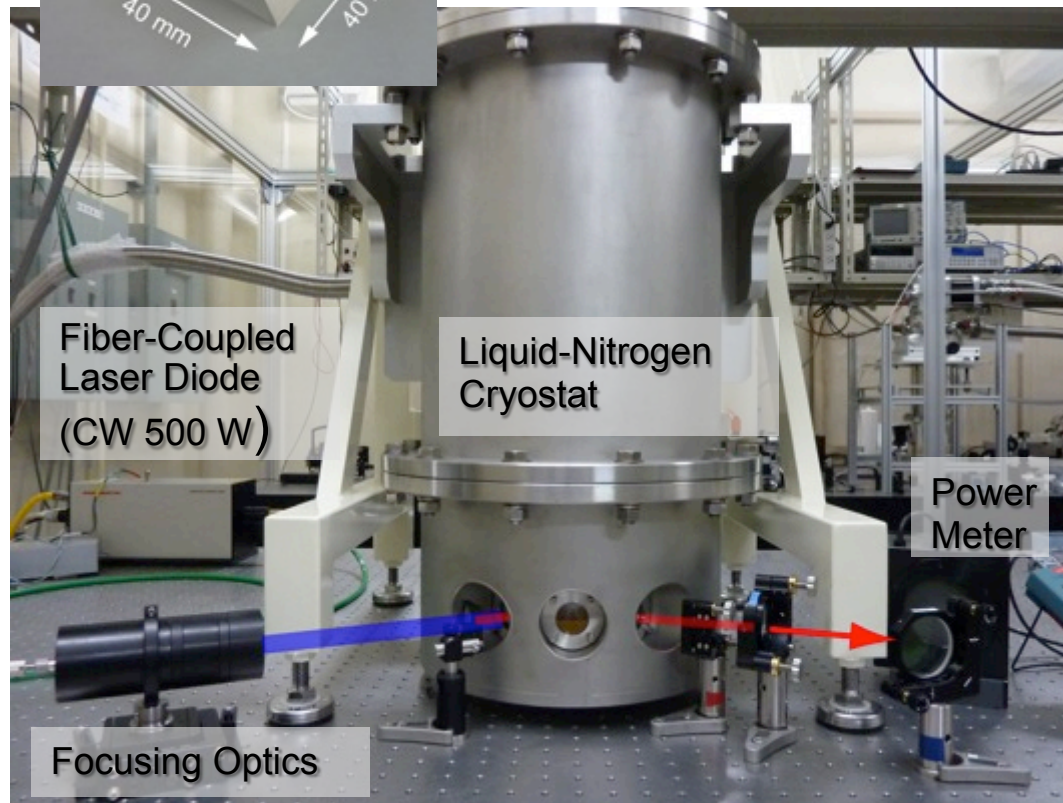
# High power multi-transverse mode **TRAM Oscillator**

**Konoshima Cemical Co. Ltd.**



Yb:YAG: **9.8 at. %**  
0.18 mm  
0.4 mm  
0.6 mm

Yb:YAG : d = **0.4 mm**



**Multi-transverse mode**

Output : **273 W**

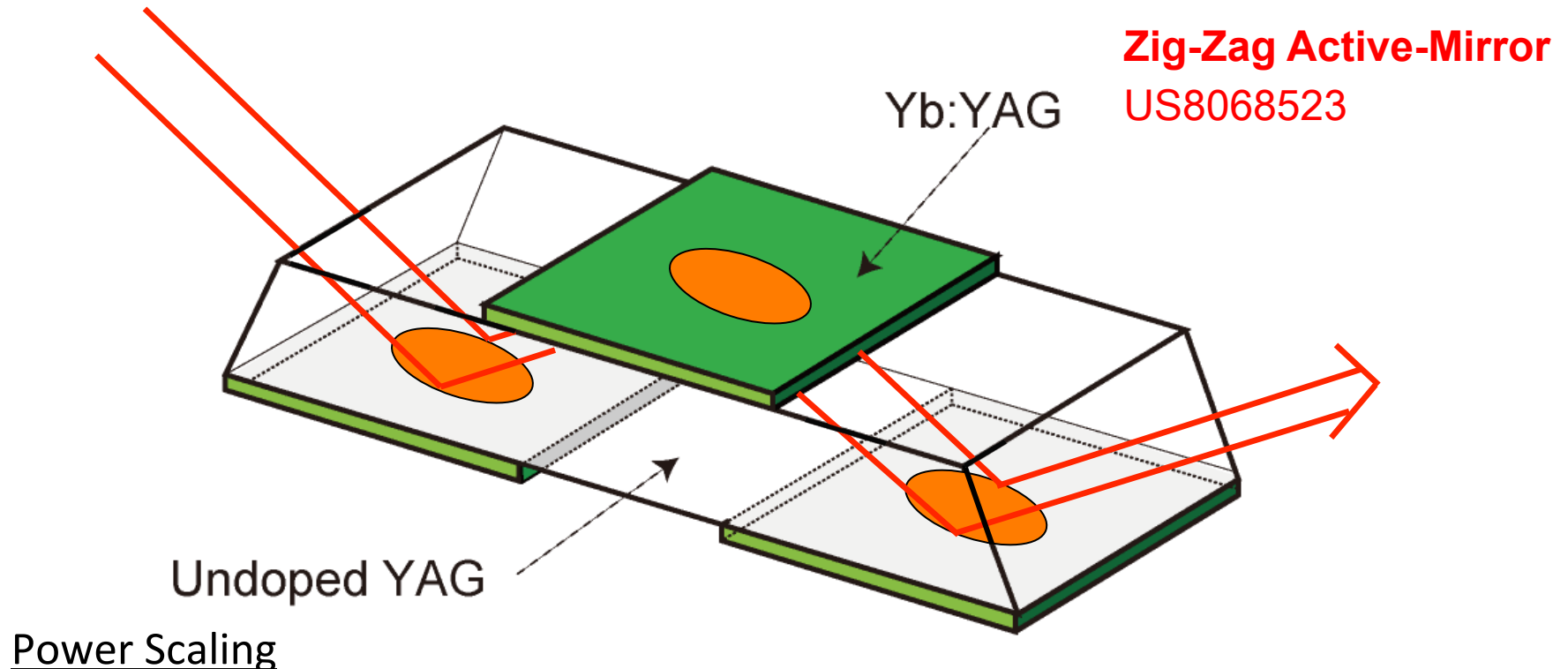
Optical Effi. : **65%**

Slope Effi. : **72%**

Pump Intensity : **0.75 kW/cm<sup>2</sup>**

H. Furuse, *et al*, *Opt. Lett.* 34, 3439 (2009).

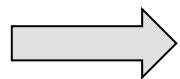
# Combining multi-TRAMs for 10 kW class laser power



Enlarged pump area + Serially arranged multi-TRAMs

## Design Concept

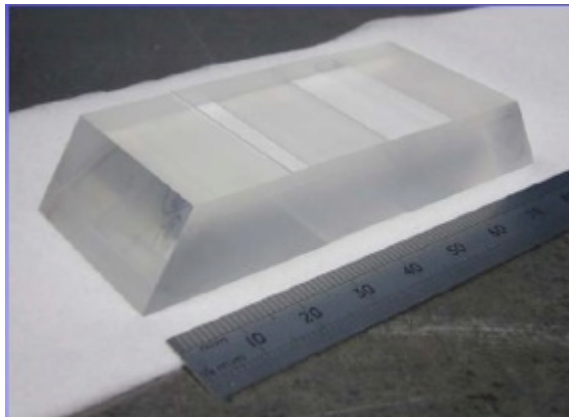
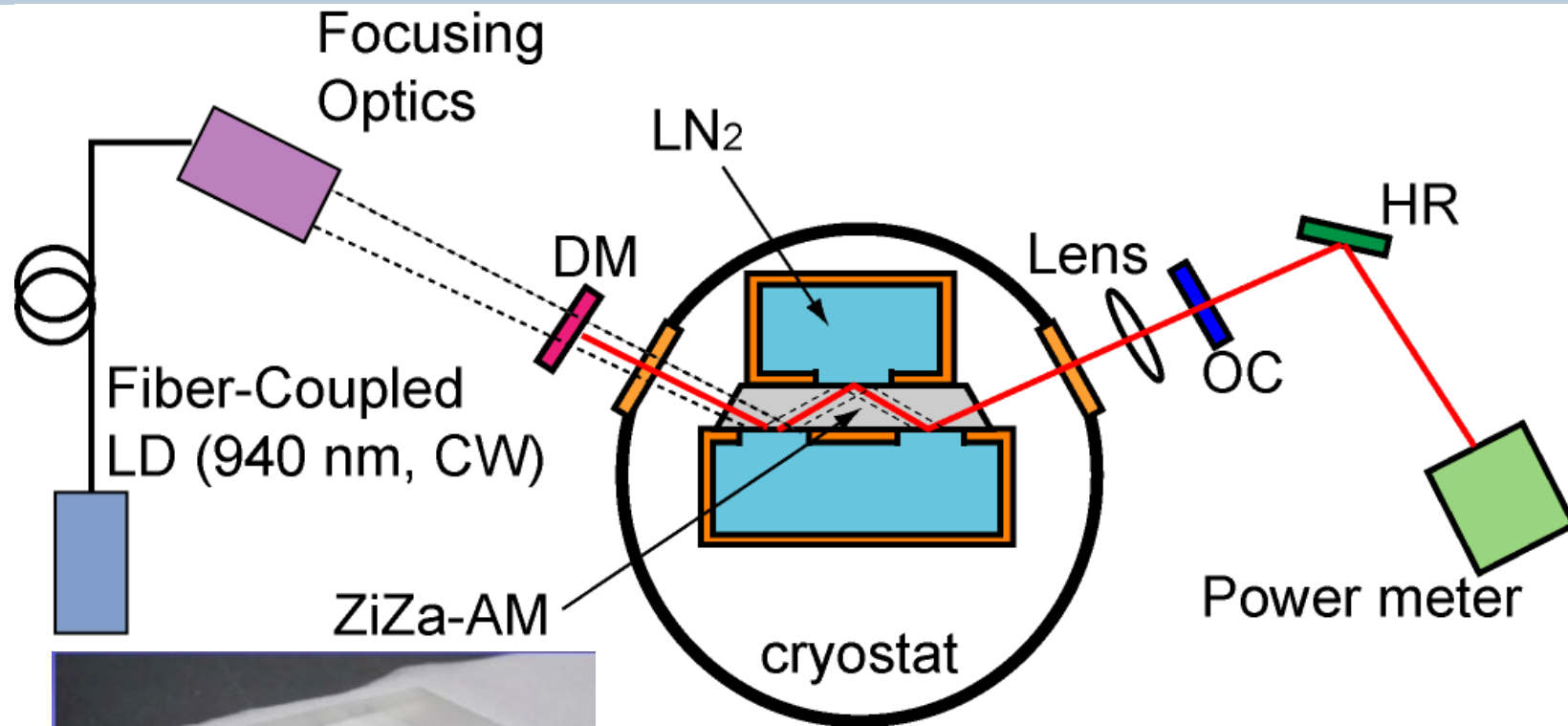
- » Each temperature rise is **almost the same** with thickness and doping.
- » More than **95%** of the pump beam can be absorbed.



*10 kW class Laser Oscillator* (for Industries)

*500 W class Laser Amplifier System* (for Pulse Operation, CPA)

# Experimental Setup for ZiZa-AM Laser Oscillation



**3 Yb:YAG disks**

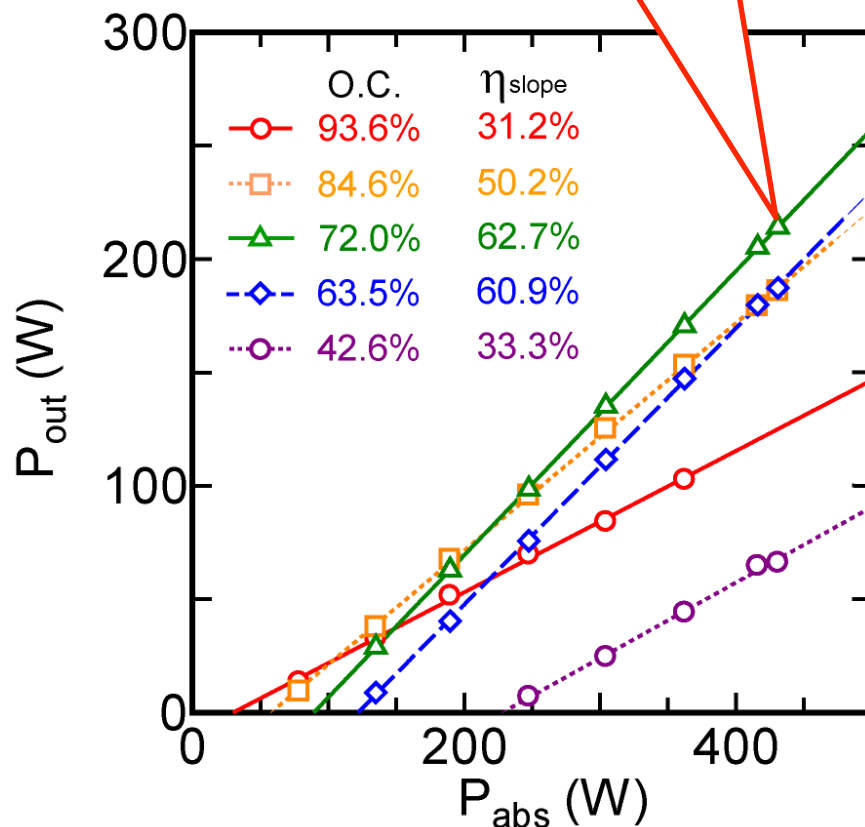
**Konoshima Cematic Co. Ltd.**

- CW 500 W LD was used as a pump source. → **431 W** was absorbed in ZiZa-AM.
- Pump beam was focused onto each Yb:YAG disk at **9 mm, 8 mm, and 9 mm**, respectively.

# Experimental Results of ZiZa-AM Laser

## Multi-transverse mode

$P_{\max} = 214 \text{ W}$   
 $\eta_{\text{o-o}} = 50\%$   
 $\eta_{\text{slope}} = 63\%$



- We have obtained **214 W** with **50%** optical efficiency and **63%** slope efficiency. These were lower than the TRAM results.

### ■ ■ ■ Because...

- ✗ The absorbed **pump intensities are very low** (142, 169, 63 W/cm<sup>2</sup>).
- ✗ The beam coupling may be poor.



Both of the laser power and the optical efficiency **will be improved with more powerful pump source**. Now, we are preparing more powerful pump LD to achieve **kW class power**.



## Approaches for higher performance

### **Multi Transverse Oscillation → MOPA System**

- Study of TRAM Amplification Characteristics

(Small Signal Gain, ASE/Parasitic Lasing, Temperature rise, Wave-front Distortion, Birefringence Losses, etc ...)

→ ***For several-kW laser systems***

(10 J and 100 Hz, 100 J and 10 Hz)

- 10 kW laser system based on ZiZa-AM concept.

→ ***For 10-kWclass laser systems***

(100 J and 100 Hz, 1 kJ and 10 Hz)



# Thermal Analyses

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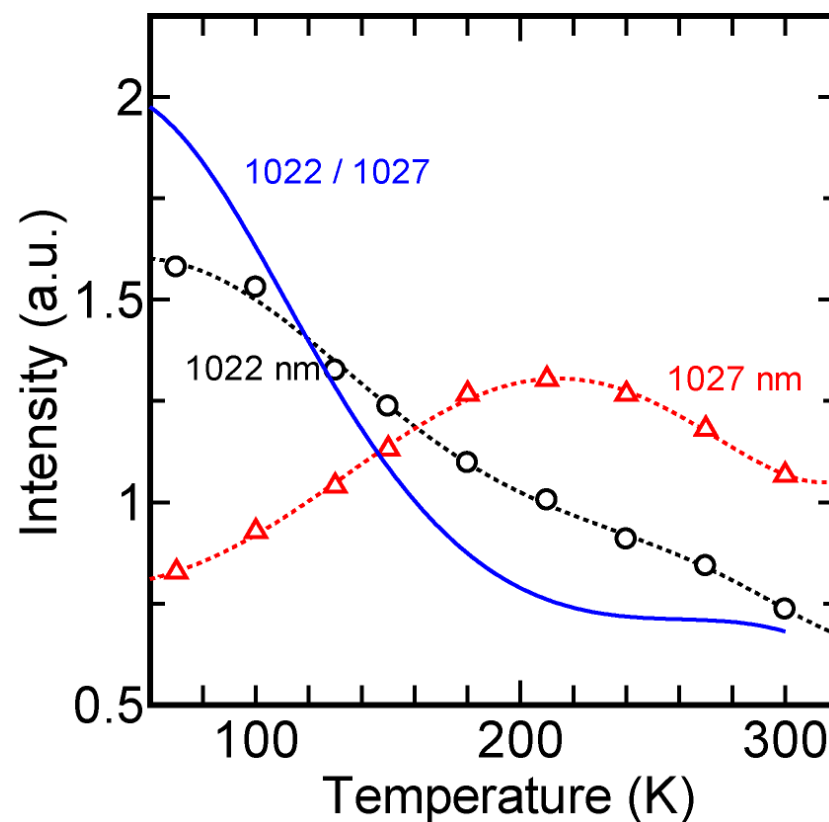
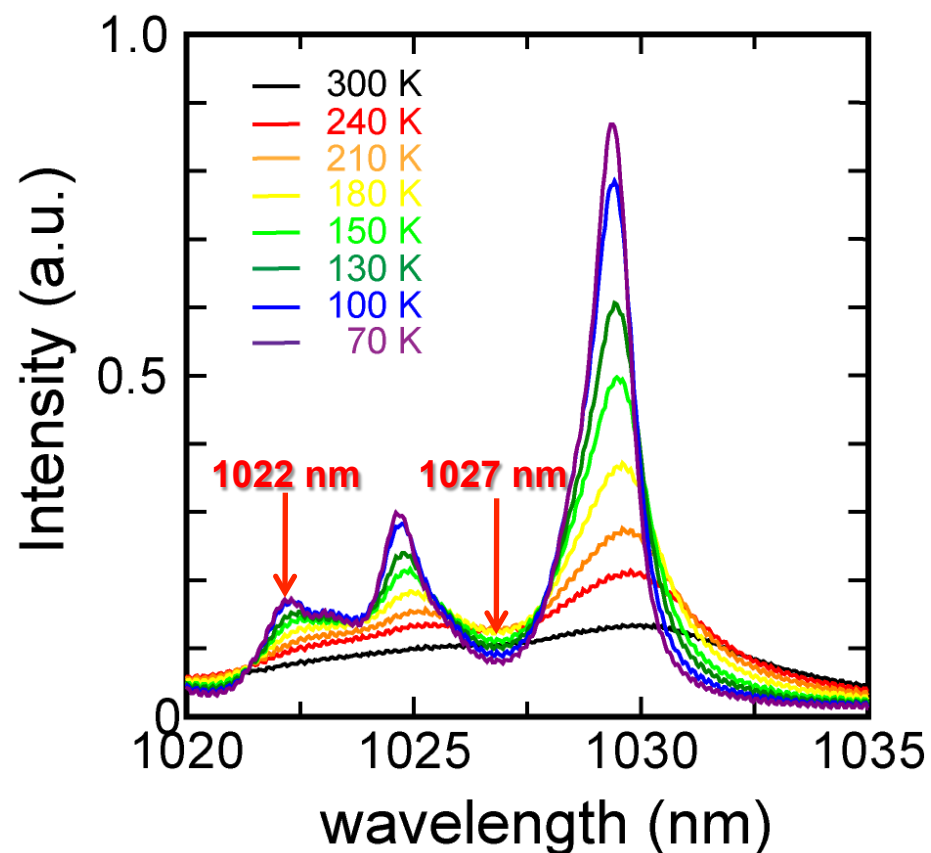
## *Experimental*

- Temperature Rise
- Wavefront Distortion
- Thermal Birefringence

## *Theoretical*

- 3D Thermal Distribution
- Thermal-Stress Distribution
- Ray Trace

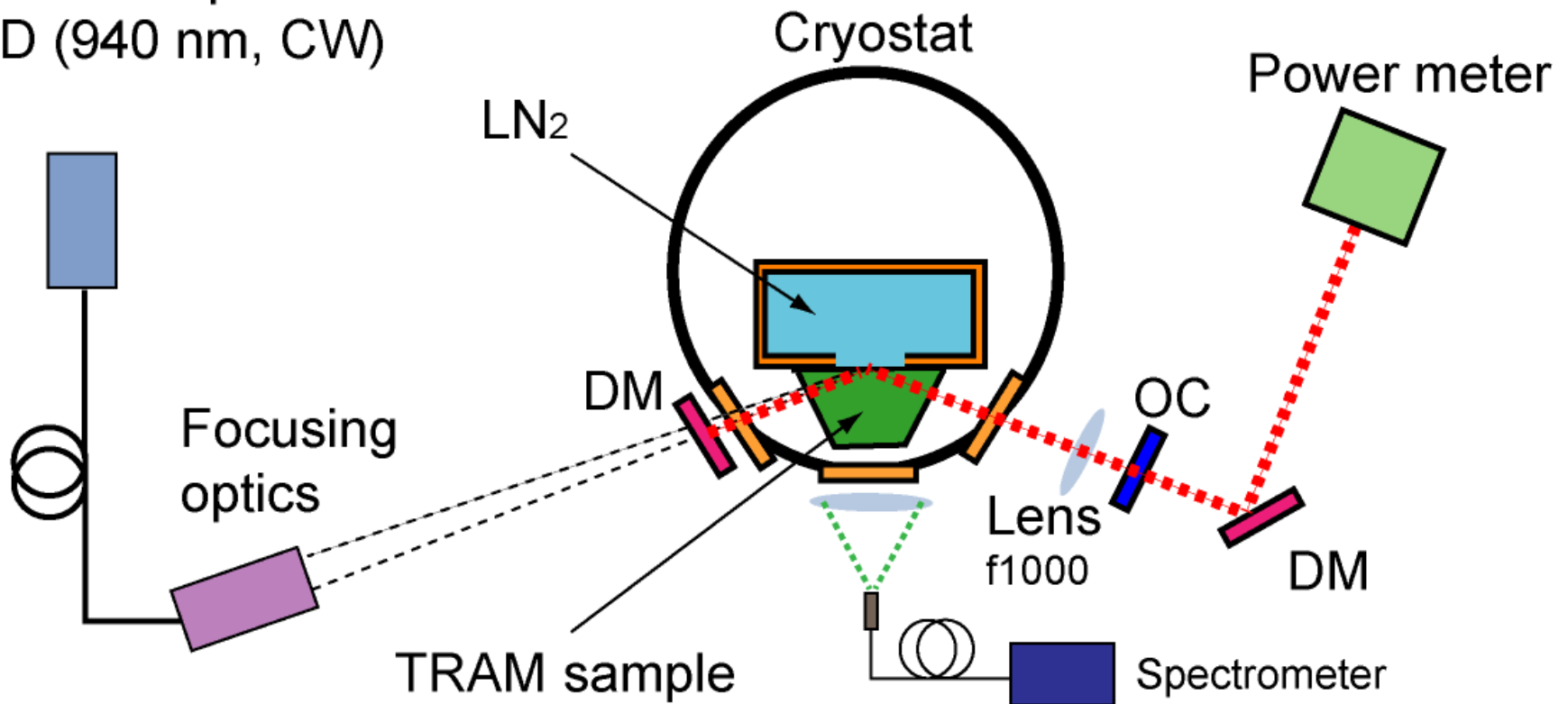
# Estimation of Yb:YAG Temperature



- Yb:YAG temperatures were inferred by comparing with **temperature controlled fluorescence spectra** which are measured by a thin Yb:YAG ceramics with low pump power to exclude re-absorption effect and temperature rise.

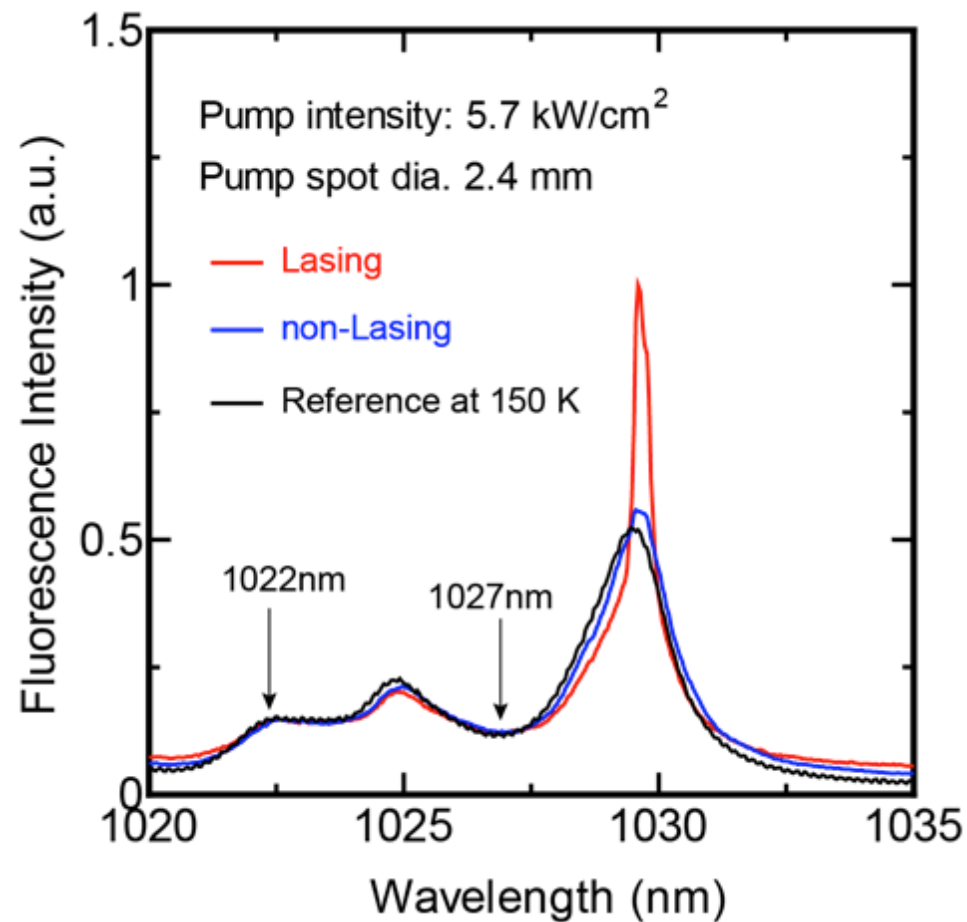
# Experimental setup for temperature rise

Fiber-Coupled  
LD (940 nm, CW)



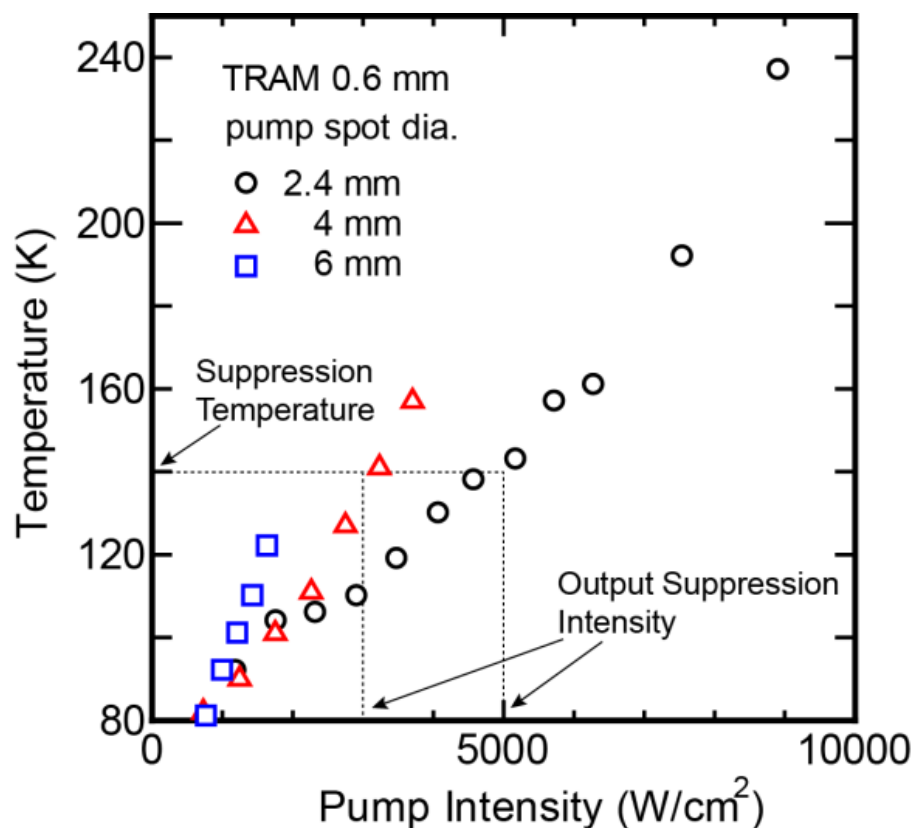
- Fluorescence spectra were also measured by a spectrometer.
- These experiments were performed under lasing and non-lasing conditions.

# Comparison of fluorescence spectra at high pump intensity



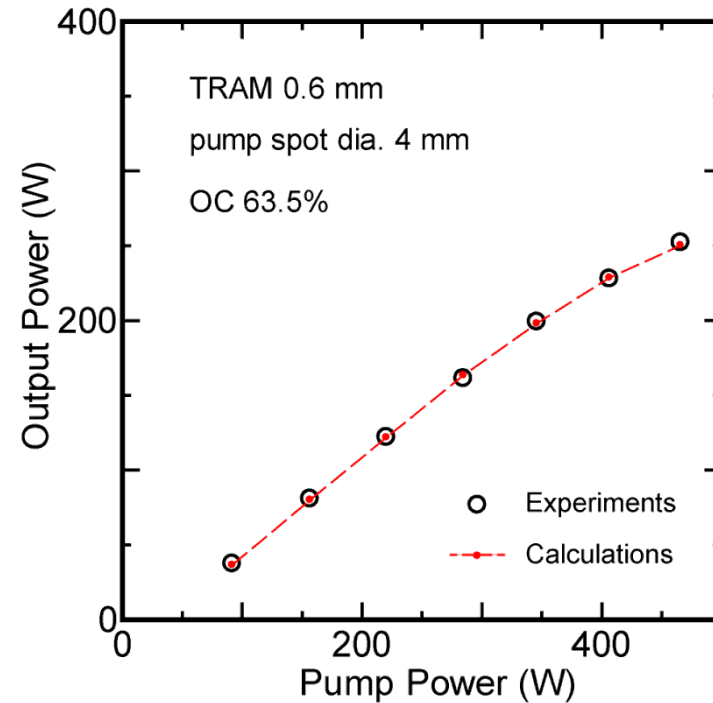
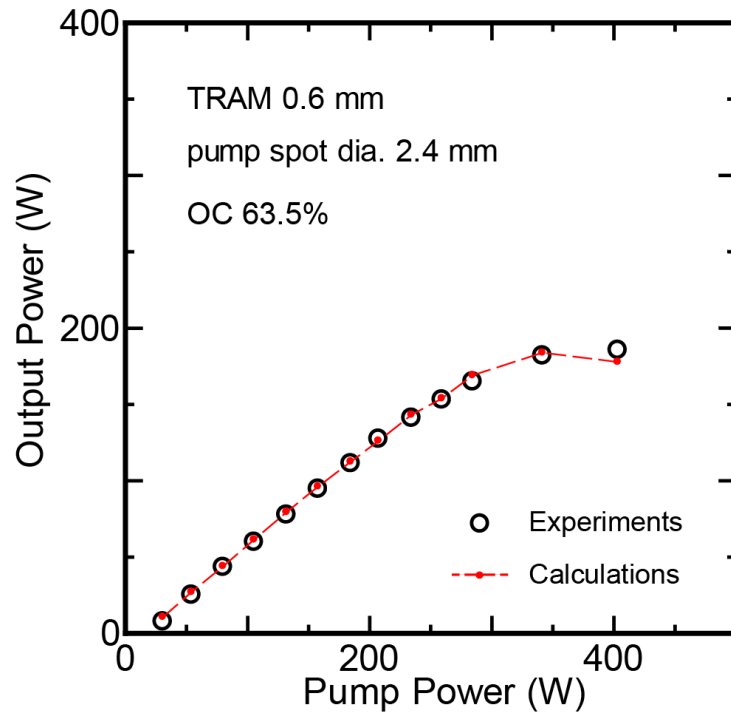
- There is a discrepancy between spectra at 1029.5 nm due to the lasing and amplified spontaneous emission, however, fluorescence intensities at 1022 nm and 1027 nm are invariant.

# Temperature Rise of 0.6mm-thick TRAM



- Yb:YAG **temperature** is **lower** for the smaller pump spot size under the same pump conditions. This is because the cooling efficiency is higher for smaller pump spot size due to omni-directional cooling.

# Output characteristics for 0.6 mm-thick TRAM

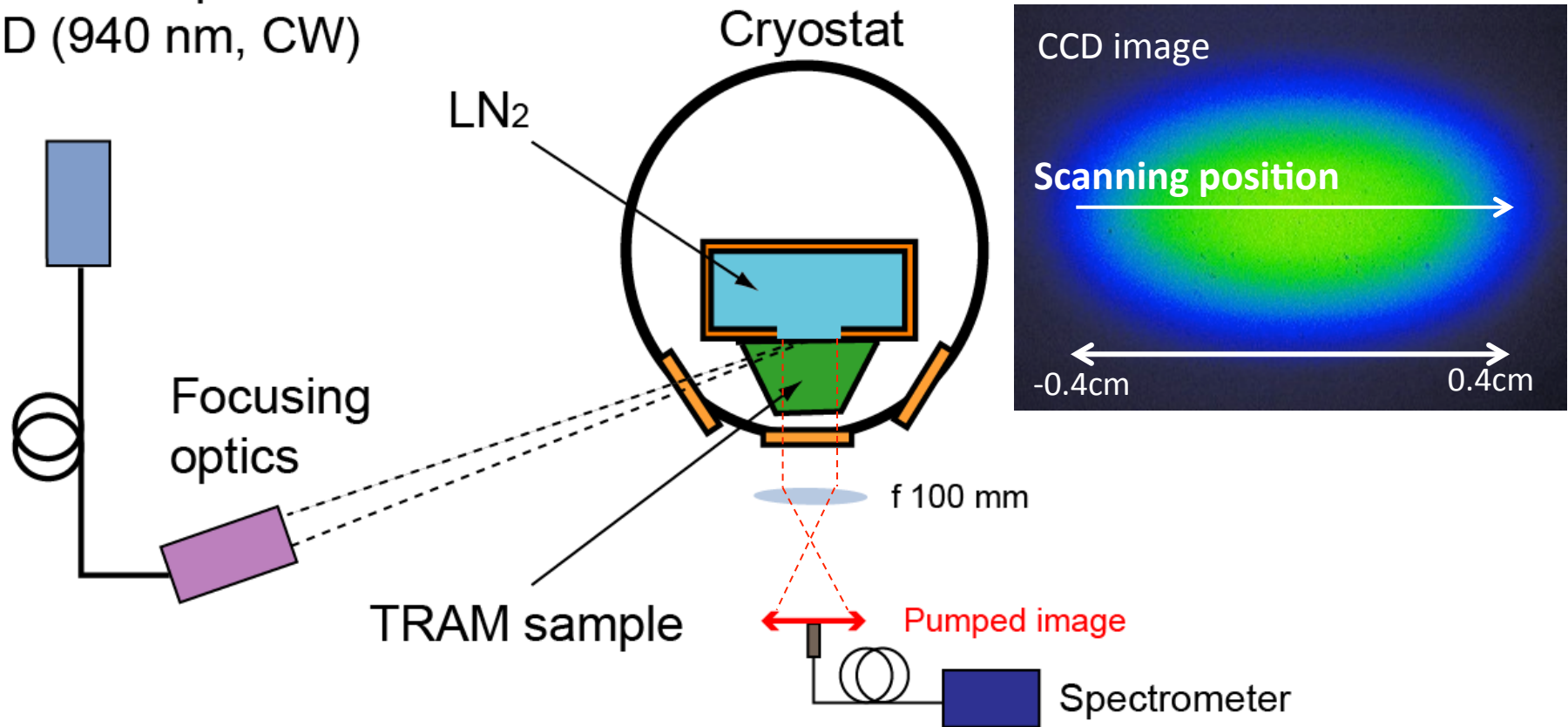


$$P_{out} = \frac{I_s(T)S}{2} \left( \frac{1-R}{1+R} \right) \left( \frac{2g_0(T)l}{\delta - \ln R + 2\alpha'(T)l} - 1 \right),$$

$$g_0(T) = \sigma_{emi}(T) \tau_f \eta_Q \eta_S \eta_a \eta_B \frac{1}{h\nu} \frac{P}{V},$$

# Thermal Distribution

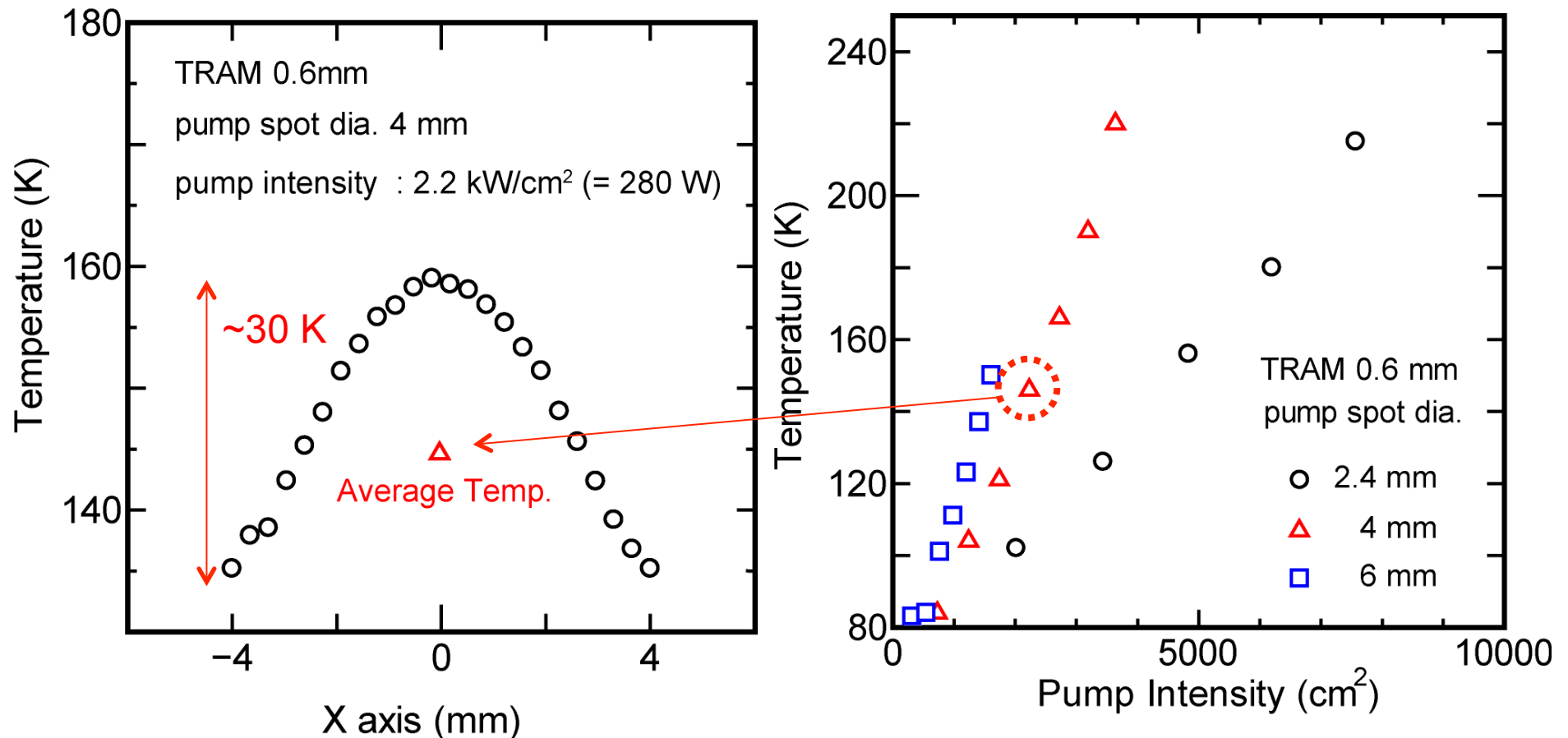
Fiber-Coupled  
LD (940 nm, CW)



- To study the thermal distribution in Yb:YAG layer, we expanded an image of the pumped area, and measured the fluorescence spectra by scanning the position.
- The pump spot diameter was 4 mm, and the pump intensity was  $2.2 \text{ kW/cm}^2$ .



# Thermal Distribution (non-lasing case)

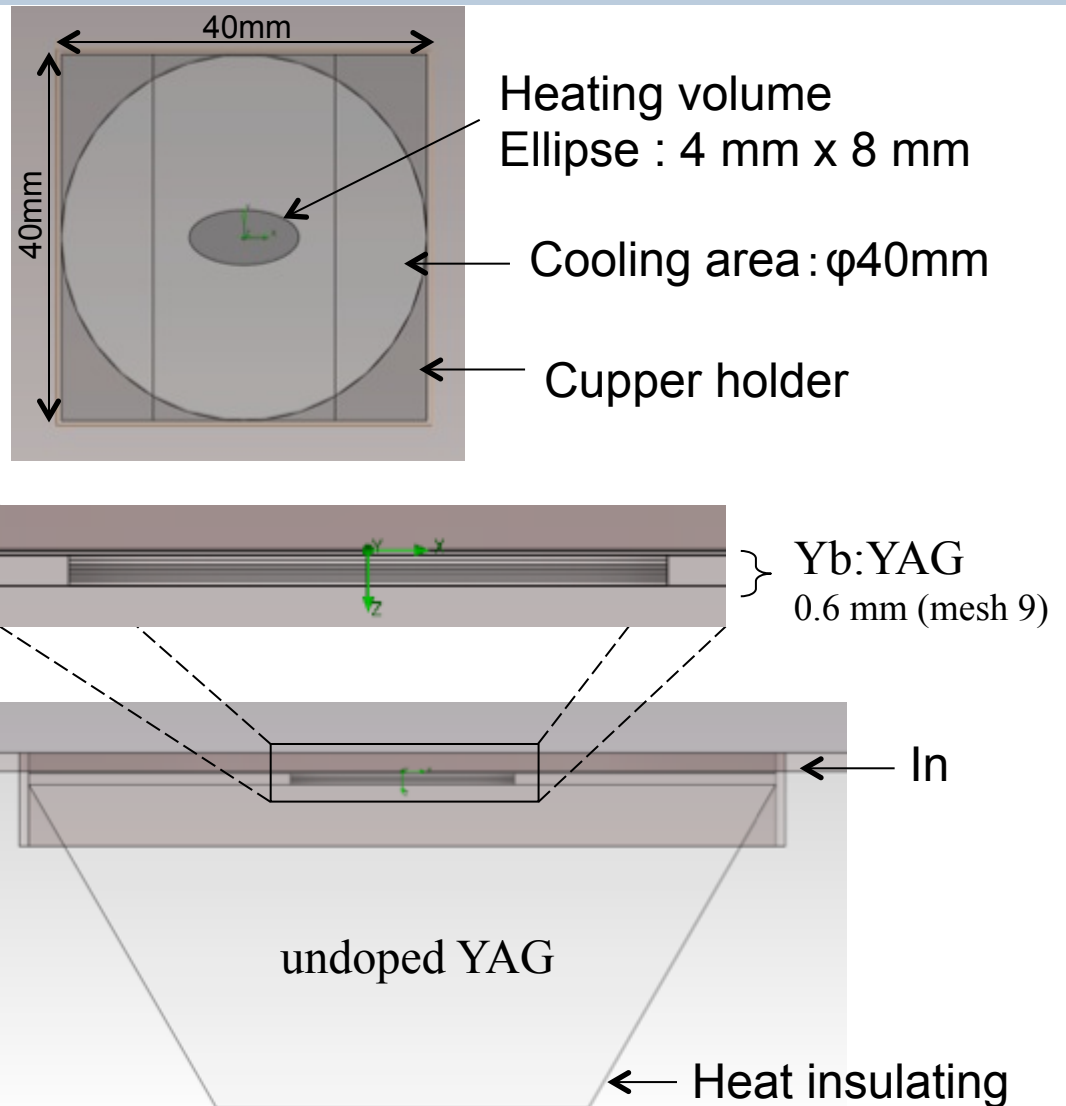
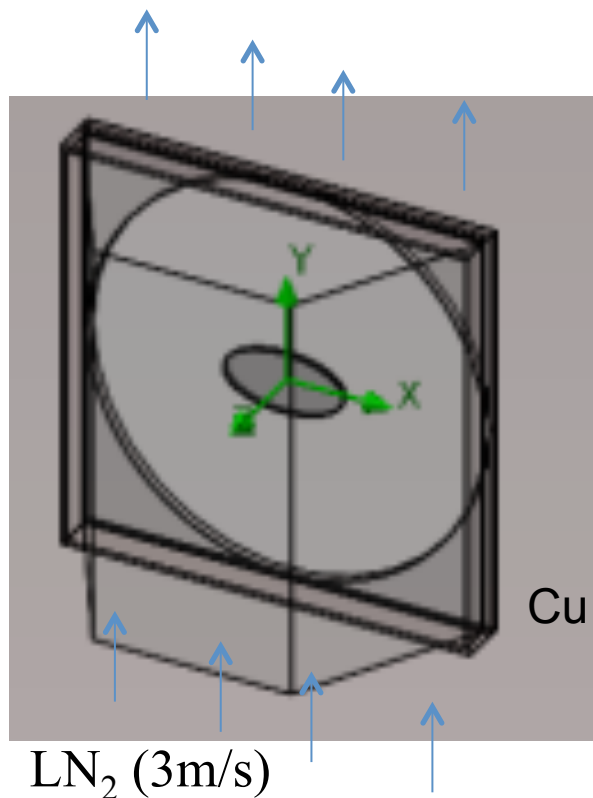


- We can see the thermal distribution in the Yb:YAG layer, and the temperature difference in the layer is about 30 K.
- The calculated temperature from a sum of the spectra approximately shows the average temperature.

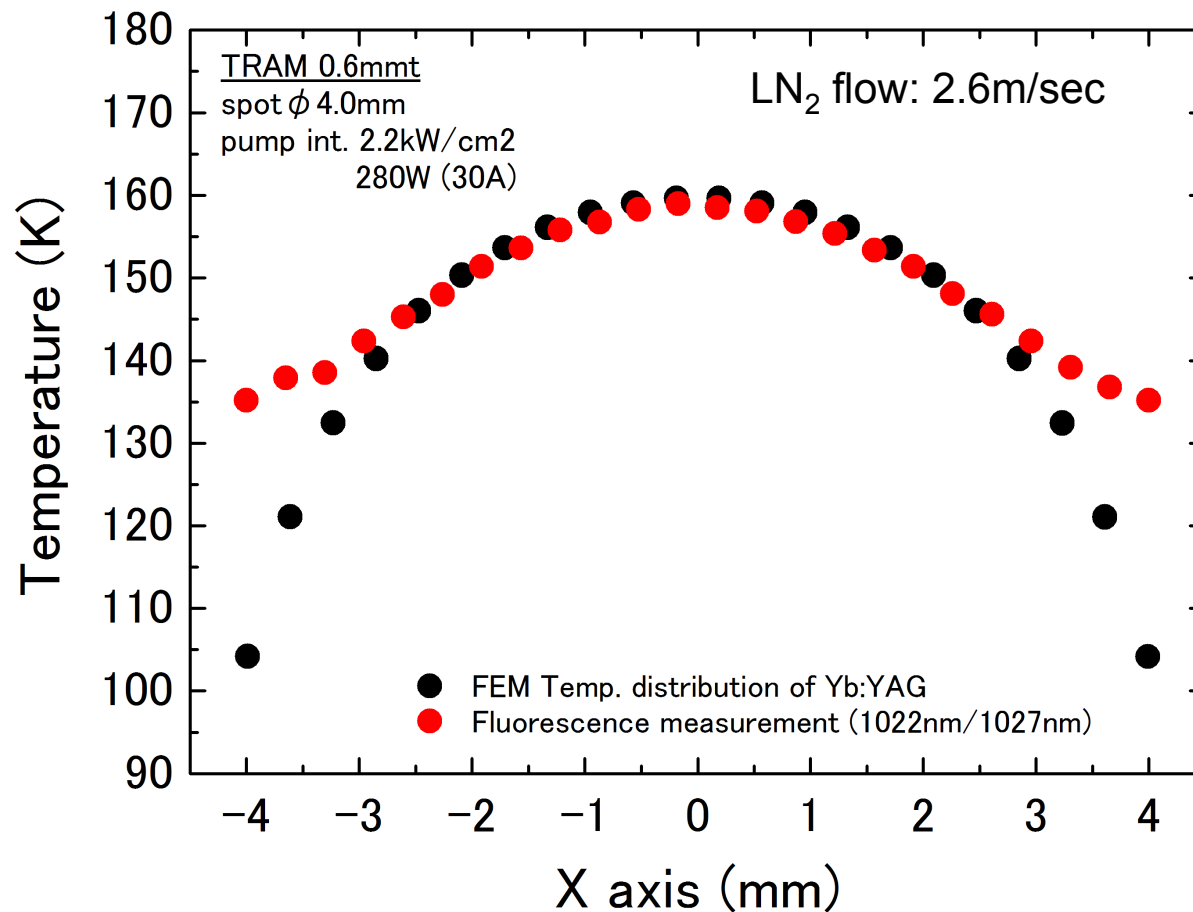
# Calculation Model

## Finite Element Method

- Mesh:  $\sim 1$  million
- $K(T)$  for undoped and doped YAG
- Coolant:  $\text{LN}_2$
- Heat generation effi. : 20%



# Comparison between Experiments and Calculations



- The calculated temperature distribution in the Yb:YAG layer using FEM shows a reasonable agreement with experiments.
- In the calculations, the heat transfer coefficient was 8600 W/m<sup>2</sup>K.

# Calculated Results and Comparison with experiments

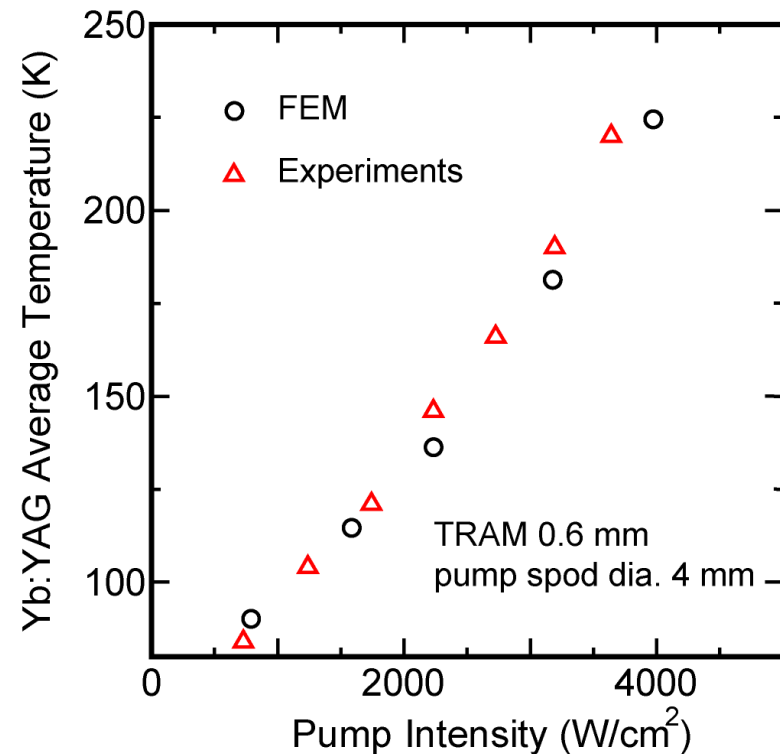
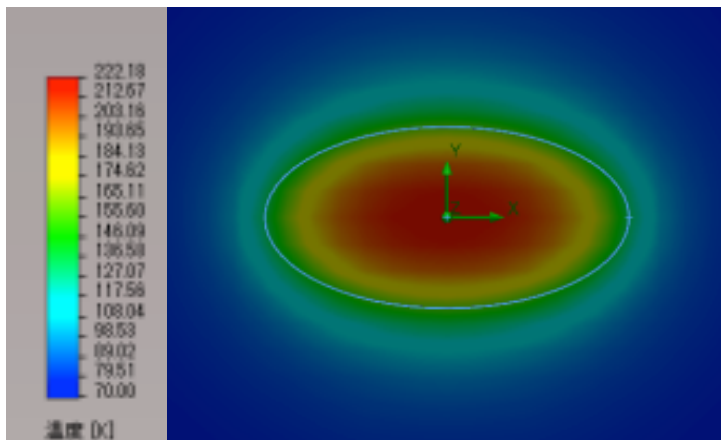
## Temperature of Yb:YAG (FEM)

Pump dia. :  $\phi 4.0\text{mm}$

Pump intensity:  $1\sim 5\text{kW/cm}^2$

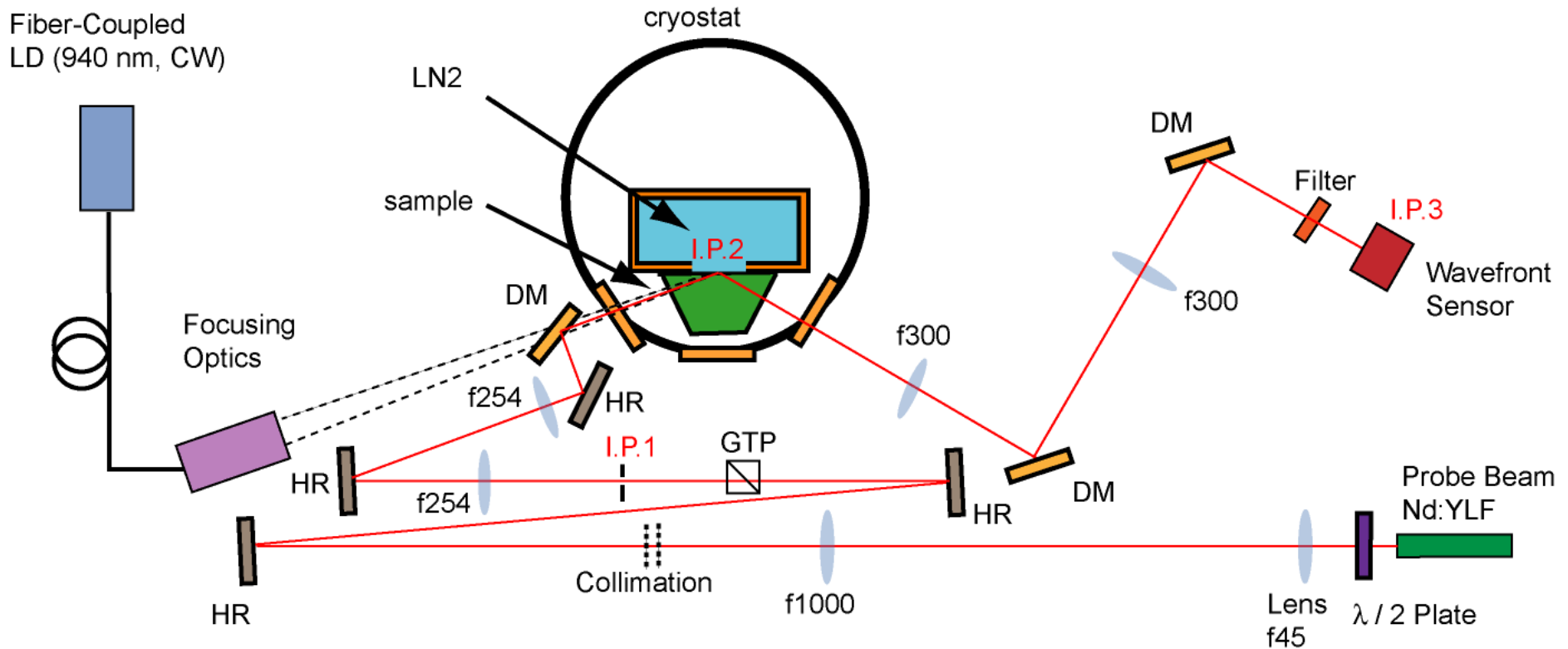
LN<sub>2</sub> flow speed:  $2.6\text{ m/s}$

example :  $1.8\text{kW/cm}^2$



- The average temperature from FEM calculations were good agreement with experiments, and we could explain the Yb:YAG temperature from calculations.
- We will calculate the Yb:YAG temperature for the case of enlarging pump, for increasing the output power.

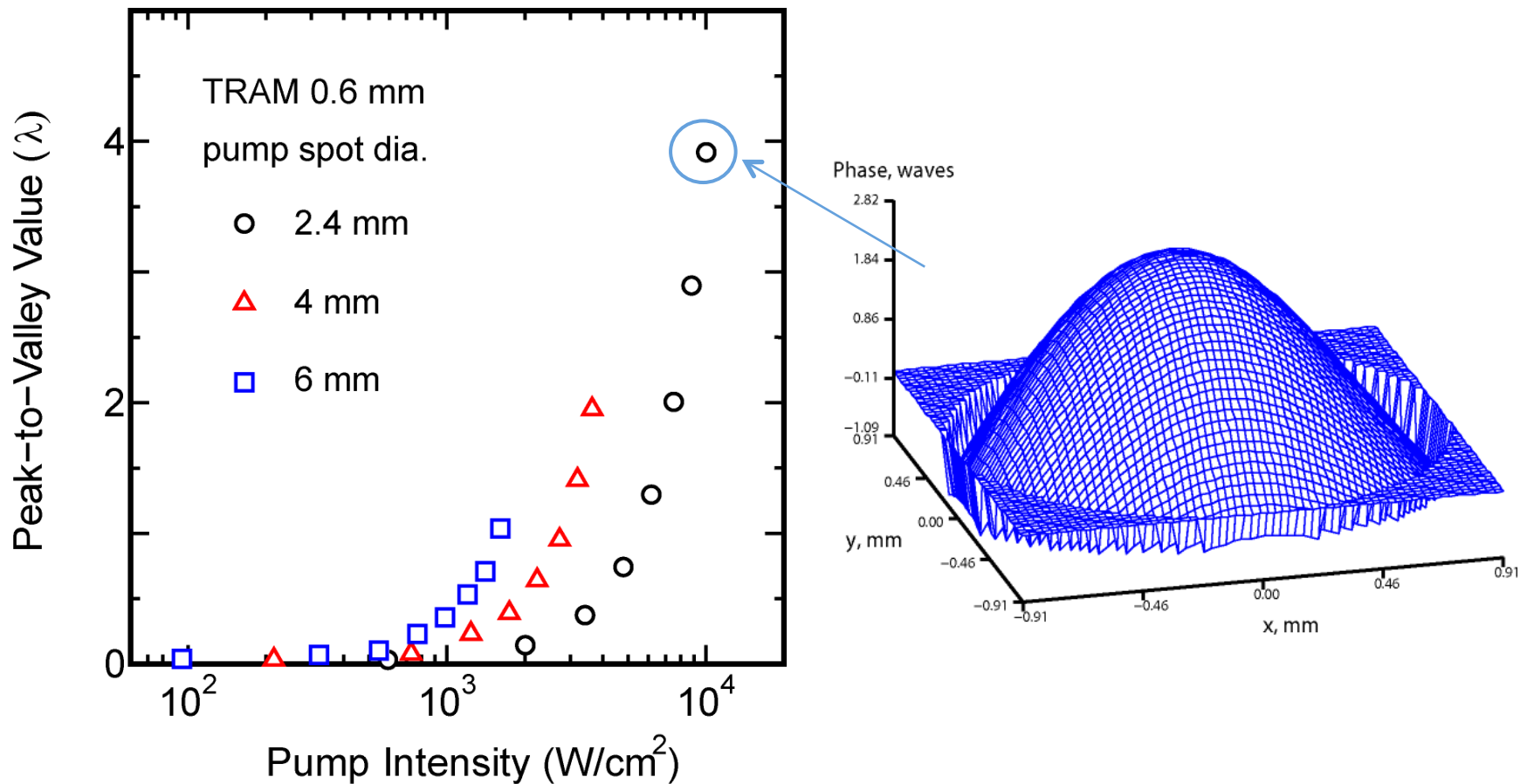
# Wave-front Measurement Setup



- A Fiber-Coupled LD (CW 500 W, 940 nm) was used as a pump source, and a linearly polarized Nd:YLF laser (CW 70 mW, 1054 nm) was used as a probe beam.
- Pump beam spot diameter on Yb:YAG TRAM was  $\sim 2.4$  mm, 4 mm or 6 mm.
- A wavefront of the transmitted beam was measured by **Shack-Hartmann wavefront sensor**.

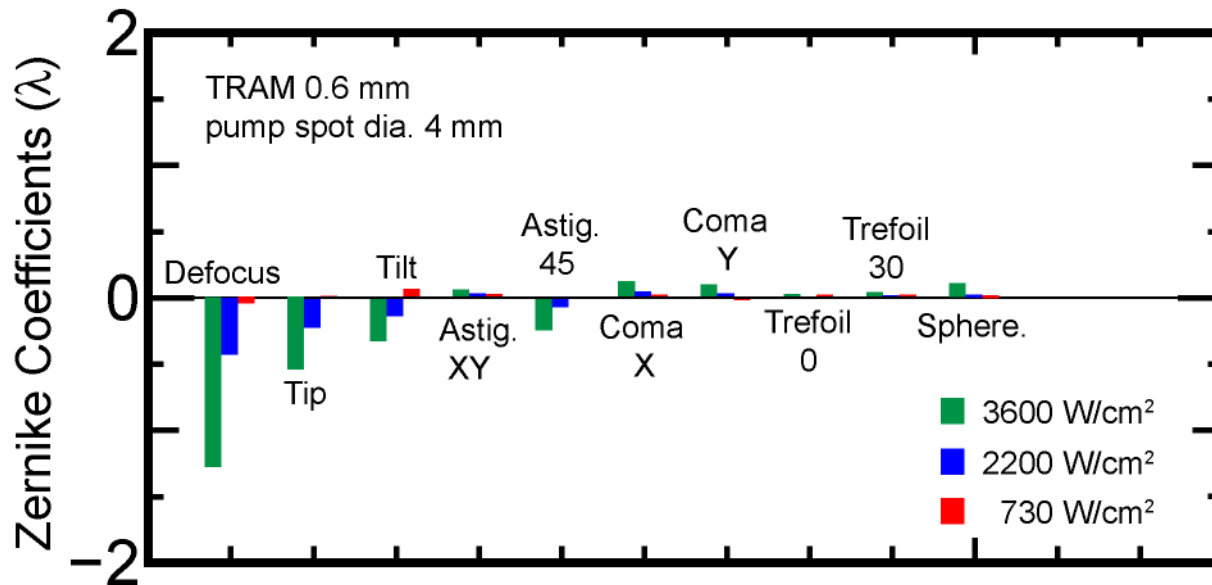
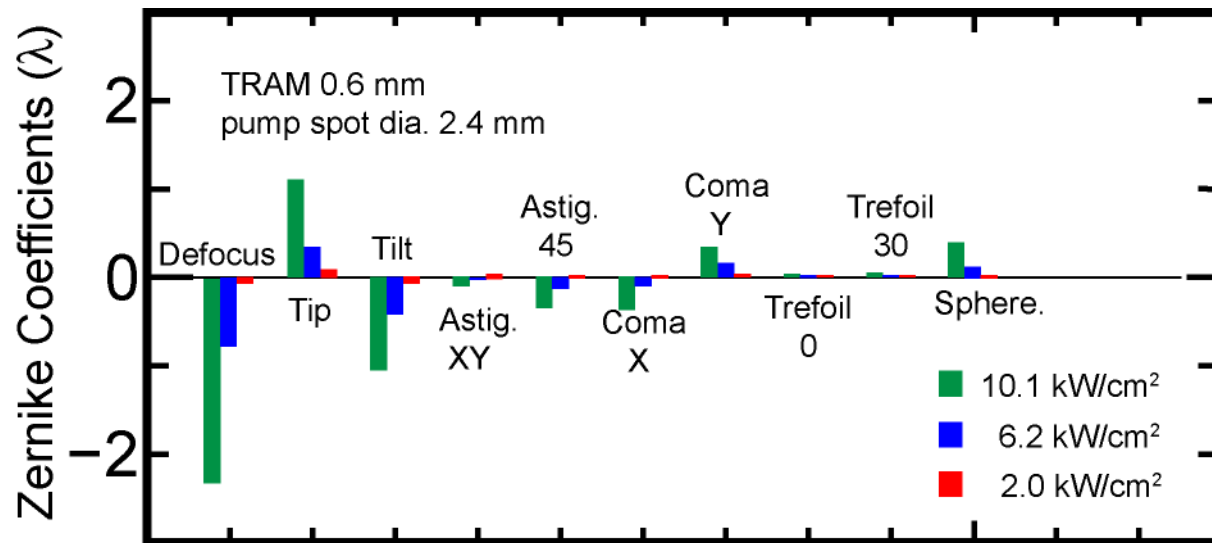
# Wave-front Distortion of 0.6 mm-thick TRAM

TRAM 0.6mm,



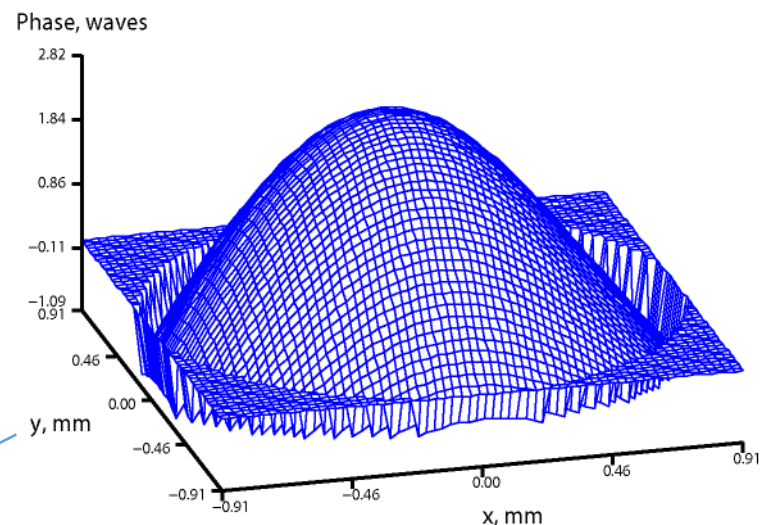
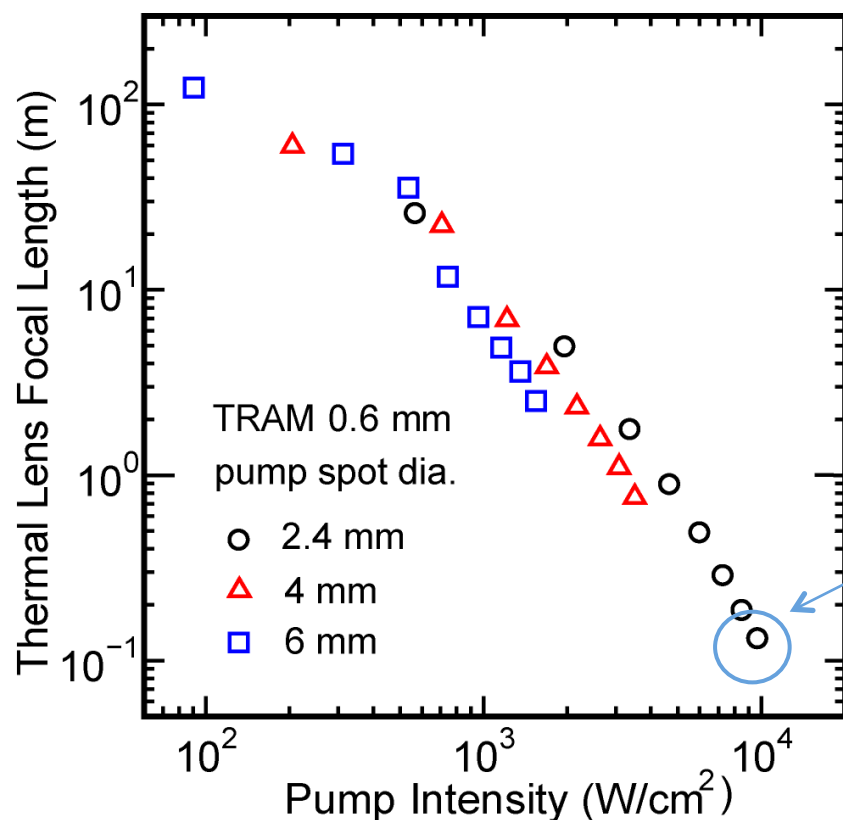
- The transmitted wave-front was measured using a **Shack-Hartmann sensor**.
- Peak to valley value was over  $4 \lambda$  at the highest pump intensity ( $10 \text{ kW}/\text{cm}^2$ ).

# Zernike Polynomials





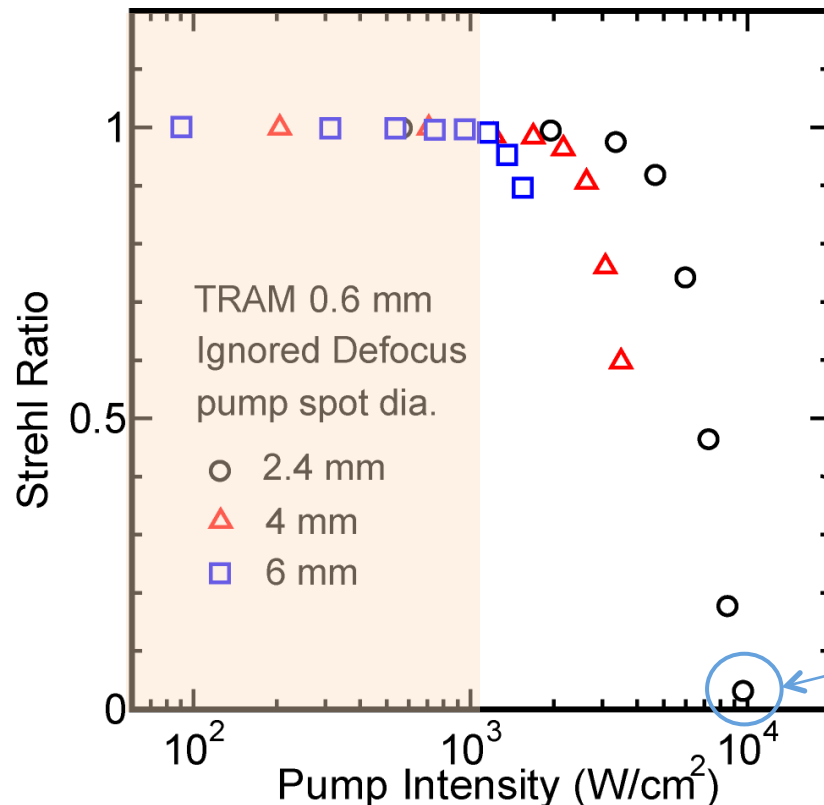
# Wavefront Distortion and Thermal Lens Effect



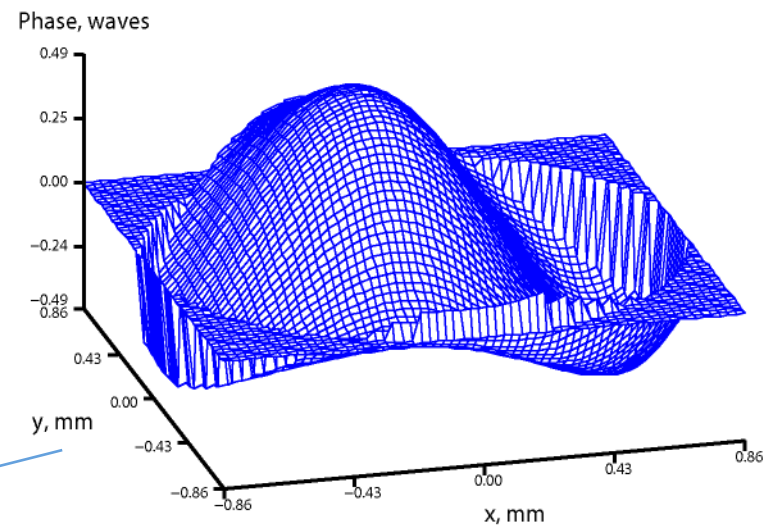
$f \sim 130 \text{ mm}$

- The phase distortion at the wave-front sensor is expanded on **Zernike polynomials**, and the **thermal lens focal length** can be estimated.
- For 0.6mm thick TRAM, the strong thermal lens effect with  $f \sim 130$  occurred.

# Strehl Ratio and Wave-front Distortion ignoring Defocus

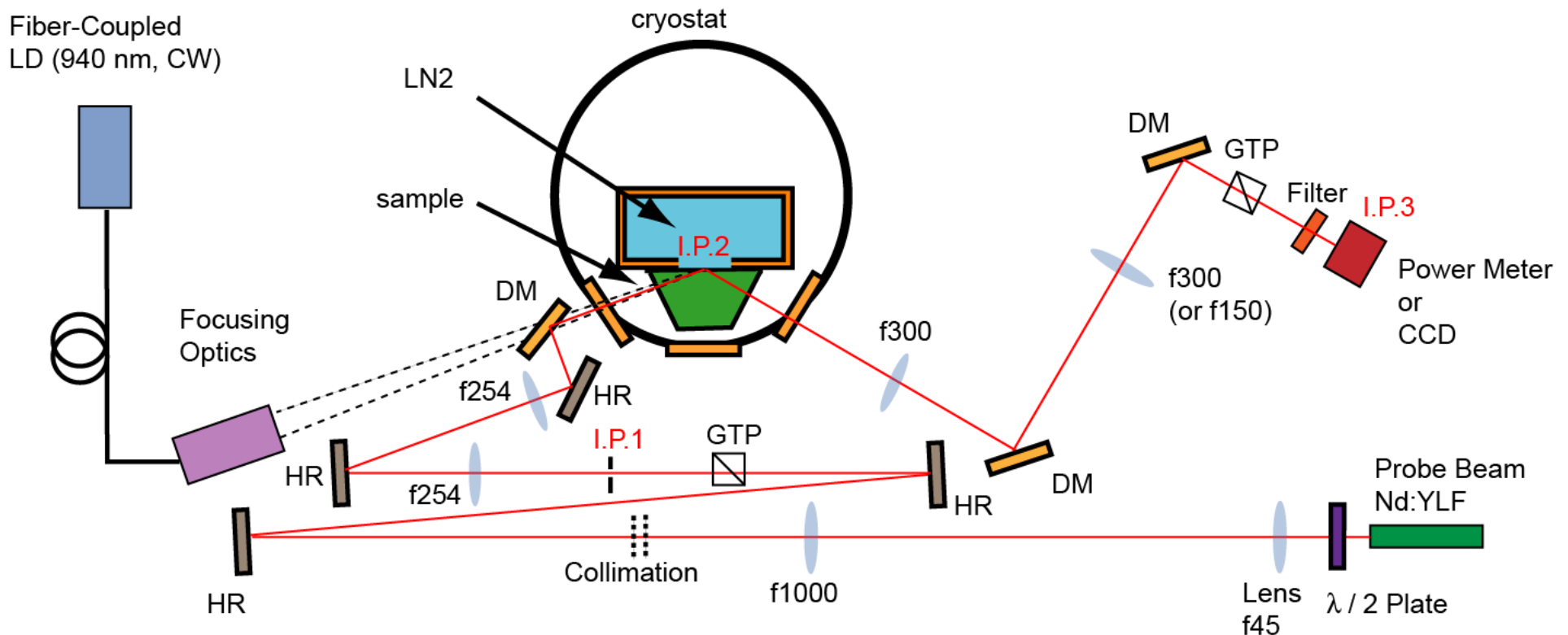


## Ignored Defocus



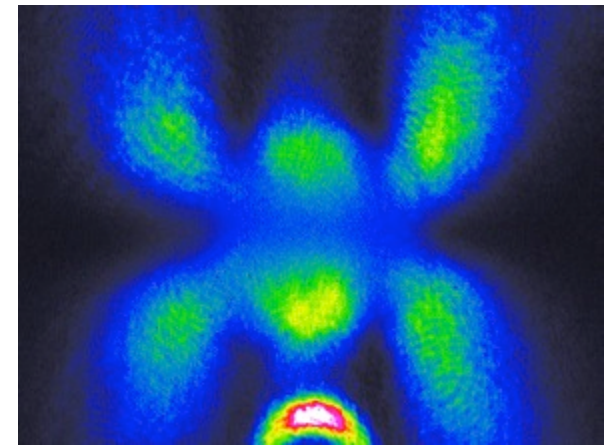
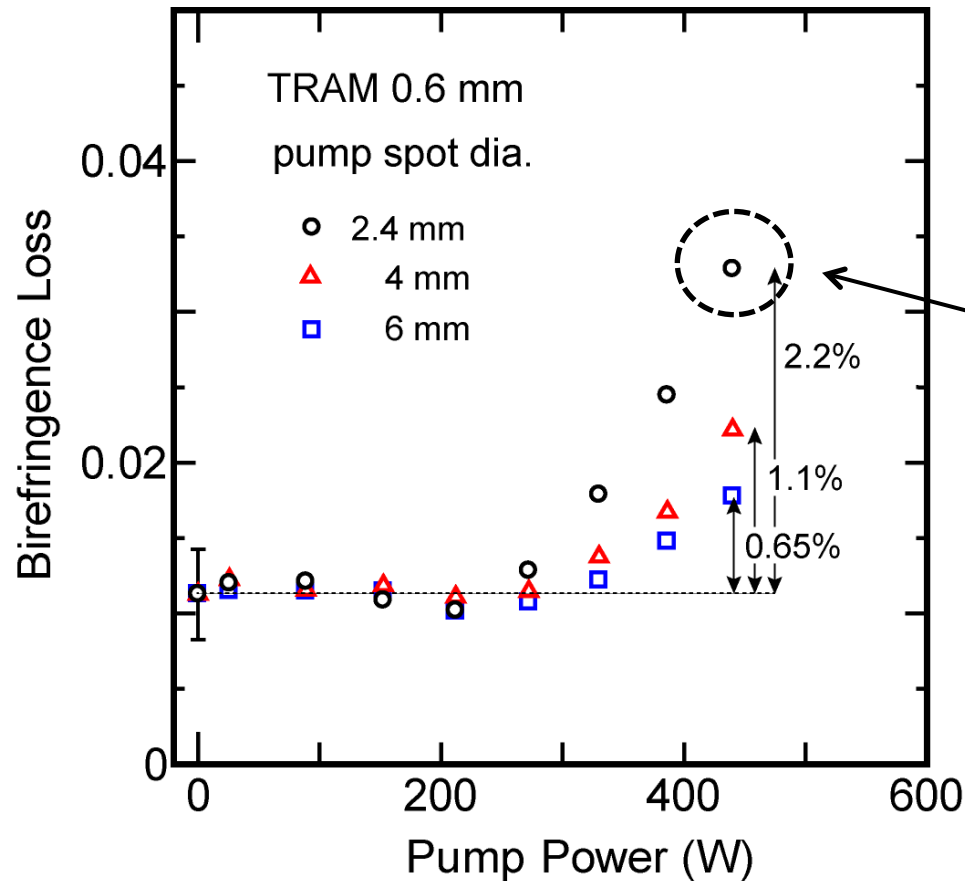
- **Defocus** component could be compensated by lenses.
- Other distortions need more sophisticated optical components such as **deformable mirrors**.
- A deformable mirror may not be necessary for up to **1,000  $\text{W}/\text{cm}^2$  pumping**.

# Birefringence Induced Loss Measurement Setup



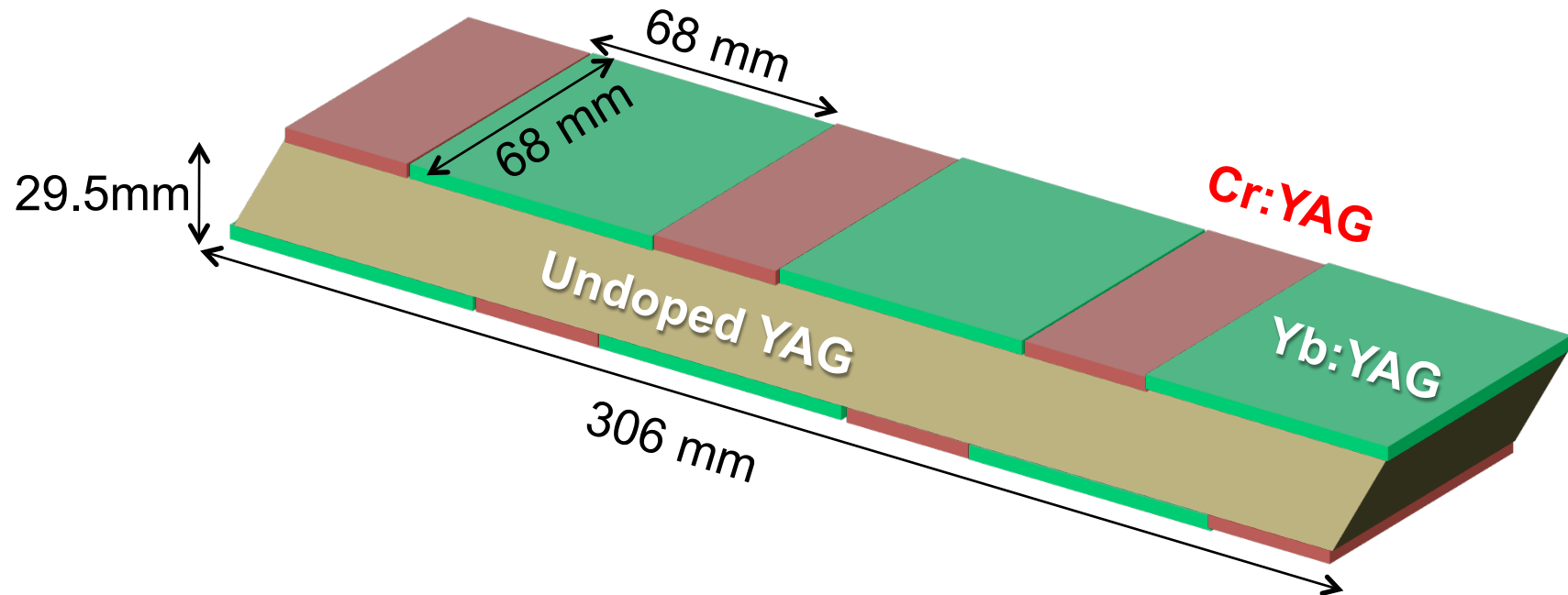
- To measure the thermally induced **birefringence loss**, Glan-Thompson polarizer pair was used under the crossed Nicol condition.
- The leakage profile and power were measured by a CCD camera and a power meter.

# Thermally induced birefringence Loss



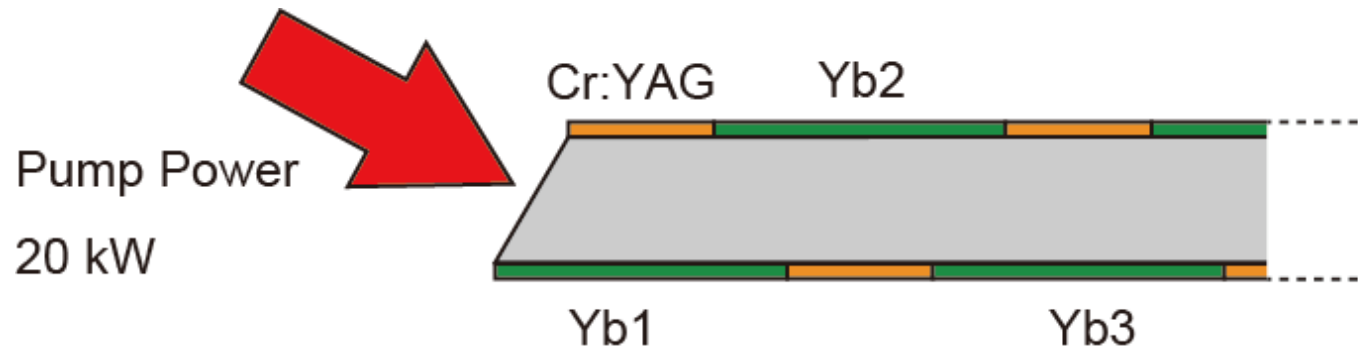
- A birefringence loss of **~ 2.2%** was observed at **~ 10 kW/cm<sup>2</sup>** pump intensity.
- The leakage pattern looks like a butterfly (the detail is under investigation).
- Experimental results will be used to compare with FEM calculations.

## Conceptual design for $> 10 \text{ kW}$ laser system



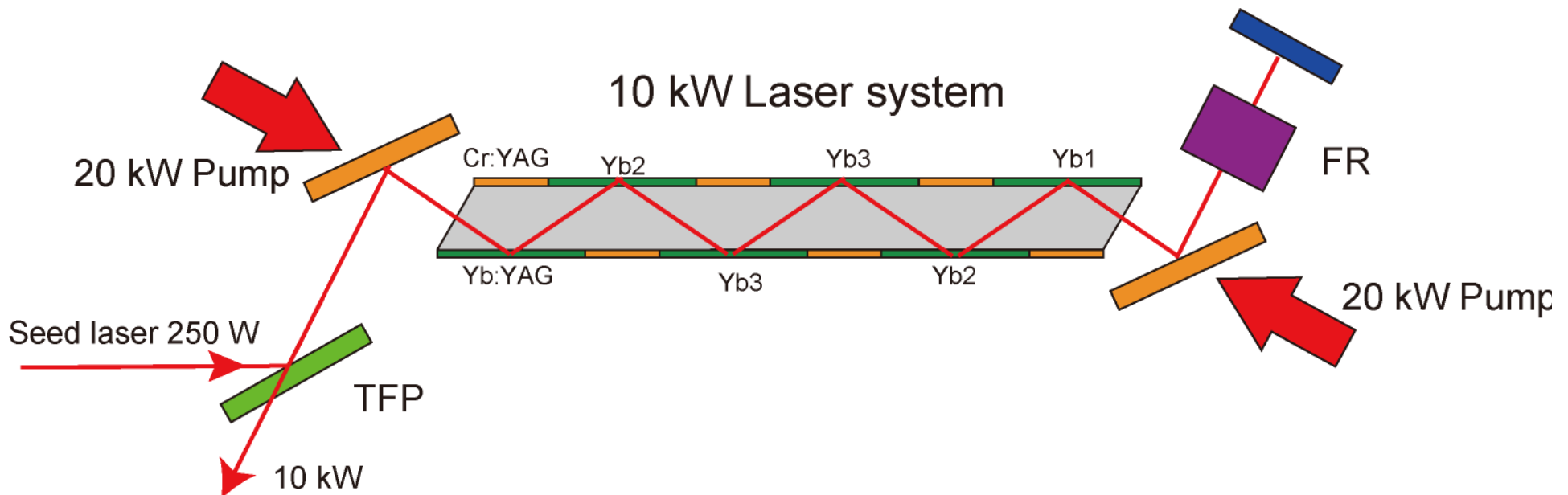
- This includes 6 Yb:YAG layers whose sizes are  $68 \times 68 \text{ mm}^2$ , and Cr:YAG layers are used as an absorber to avoid ASE effect.
- Doping concentration and thickness of each layer are adjusted to satisfy
  - Absorption : 100%
  - ASE gain :  $g_0 I_{\text{ASE}} < 4$
  - Absorbed pump Intensity :  $< 400 \text{ W/cm}^2$
  - temperature rise inside the Yb:YAG layer :  $\Delta T < 15 \text{ K}$ .

# Conceptual design for $> 10 \text{ kW}$ laser system



	Yb1	Yb2	Yb3	Requirements
Doping of $\text{Yb}^{3+}$	0.3%	0.7%	2%	
Yb:YAG thickness	2.6 mm	2 mm	2 mm	
Absorption	32.7%	34.8%	32.5%	100%
Absorbed pump power	6.5kW	6.9 kW	6.5 kW	
Absorbed pump intensity	141 W/cm <sup>2</sup>	148 W/cm <sup>2</sup>	141 W/cm <sup>2</sup>	< 400 W/cm <sup>2</sup>
$\Delta T$	10.5 K	7.7 K	11.7 K	< 15 K
$g_0 I_{\text{ASE}}$	3.0	4.0	3.8	< 4.0
Small signal gain , $G$	1.37	1.40	1.37	

## Conceptual design for $> 10 \text{ kW}$ laser system



- This can totally absorb **40 kW** of pump power and double pass gain will be  $G > 40$ . Output power of over **10 kW** ( $= 200 \text{ W/cm}^2$ ) can be possible using **300 W class seed source** and double pass amplifier.



# Summary

## ◆ Multi-transverse mode Oscillation

- TRAM . . . . .  $P_{\text{out}} = 273 \text{ W}$ ,  $\eta_{\text{o-o}} = 65\%$ ,  $\eta_{\text{slope}} = 72\%$
- 3-TRAMs (ZiZa-AM) . . .  $P_{\text{out}} = 214 \text{ W}$ ,  $\eta_{\text{o-o}} = 50\%$ ,  $\eta_{\text{slope}} = 63\%$

## ◆ Amplification Characteristics (TRAM)

- Temperature Rise . . . . We obtained temperature distribution in Yb:YAG layer
- FEM . . . We obtained reasonable agreement with experiments.
- Wavefront Distortion . . . Aberration free at  $I_{\text{abs}} < 400 \text{ W/cm}^2$
- Birefringence Loss . . . Thermally induced birefringence loss is about 2%  
at  $10 \text{ kW/cm}^2$  pumping.

## ◆ Thermal analyses of 10 kW ZiZa-AM laser using FEM

- Thermal-Stress Distribution, Ray trace → Beam profile, power potential